

INFLUENCE OF TEMPERATURE AND STRAIN RATE ON THE TENSILE BEHAVIOR OF EPOXY REINFORCED WITH CARBON NANOTUBES

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Abstract. *The purpose of this work is study the behavior of an adhesive composite diglycidyl ether of bisphenol A (DGEBA) reinforced with carbon nanotubes. Tensile tests were performed under three temperatures (25°C, 50°C and 75°C), varying the strain rate (0.5mm/min, 5.0mm/min and 50mm/min). It was shown the effect of temperature and strain rate on the behavior of the composite. Stiffness and ultimate tensile strength decrease with temperature while they are directly proportional with strain rate. The experimental results are analyzed to illustrate this. In further work, an analytical expressions based on the curves obtained on this work would be desire to propose a modeling for ultimate strength and Young's modulus as function of temperature and strain rate*

Keywords: epoxy, temperature, tensile test, strain rate, modeling

1. INTRODUCTION

There is a growing use of polymers in different fields of industry such as aerospace, automotive and petrochemical (Reis, *et al.*, 2012), because of its low cost and weight and facility of manufacture and processing (Reis, *et al.*, 2015). Maintenance and repair of ducts, pipes and others structures represent great cost on industry (Amorim, 2015). The role of polymer adhesives is getting essential on structural applications, protective coatings and reparability, especially on petroleum industry, where the welded structures have shown unwilling, since the weld process causes metallurgical transformations and concentration of residual stresses. Besides, from time to time the weld joints show crack, due to the aggressive and corrosive environment they are exposed (da Silva, 2007).

In order to override this method, petrochemical industries have used adhesive polymers and their composites. Currently, the epoxy resin is widely used in adhesives and as matrix composites, such as Bisphenol A epoxy, due to its easiness of shaping and its excellent adhesive, mechanical and thermal properties (Gonzalez-Garcia, *et al.*, 2005). Since mechanical properties of carbon fiber are engineered, being the most resistant reinforcing fiber, and at room temperature it is not affected by humidity or aggressive means like acids (Callister, 2008), its usage as fiber phase on composites has increased and the necessity to know better its interaction with resin matrix is needed (Reis, *et al.*, 2013). Mechanical properties of composites is determined by both fiber and matrix phases. Not only the properties of it single material have great influence, but also the size and disposition of the fiber, i.e. the interface fiber/matrix affects the properties of the final composite (Dilsiz and Wightman, 1999).

Yet those properties are sensitive to temperature and strain rate at which the composites are loaded (Reis, *et al.*, 2012). Until today there are few studies and information available about the effects of strain rate and temperature on adhesives composites. The stiffness and strength on composites materials normally drops with temperature rise, and decrease even more when temperature exceeds the glass transition temperature (Bai, *et al.*, 2008). It is reported (Harding, 1992) that as the strain rate goes higher, the ultimate strength increase.

In this present paper, the effect of temperature and strain rate on the behavior of DGEBA adhesive reinforced with carbon nanotubes is analyzed through tensile tests. The experimental results are presented to show the influence of temperature and strain rate on the strength and Young Moduli of the material. Next analytical expressions are proposed for those parameters as functions of strain rate and temperature. The results obtained with the analytical expressions are compared with the experimental ones.

2. MATERIALS AND METHODS

2.1 Materials

The adhesive composite has a matrix phase of diglycidyl ether of Bisphenol A (DER 331, EEW=190) from *Dow Química S.A.*, and fiber phase of single-wall carbon nanotubes (Baytubes C-150 CP) from Bayer, with diameter varying from 0.4-3.0 nm, and a concentration of 5%. The merger process was: dispersion at high speed with grinding mill. A curing agent of polyamides was used with a mix ratio 100:43. The dispersion of nanotubes in the epoxy matrix was observed on a SEM is shown on “Fig. 1”. It was dd a voltage of 5kV with a zoom varying from x8000 to x15000.

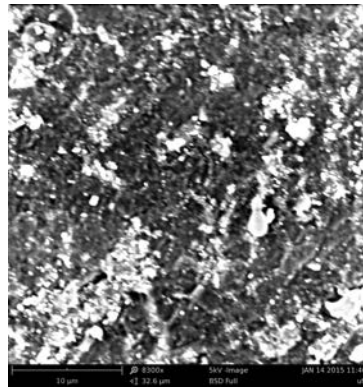


Figure 1. Example of picture taken by SEM, the white reflection represents the nanotubes.

From the *Dow Química* technical report, DER 331 is the most used liquid epoxy resin, since it applications are wide: adhesives, automotive coatings, casting, composite etc. It is also used as a standard for composites and others variations. According with Morell *et al.* (2009), DGEBA Young’s modulus and glass transition temperature are 3.8 GPa and 116°C, respectively; more properties are presented on “Tab. 1” according to manufacturer. The Baytubes are used to increase Young Moduli and hardness on composite. According to the manufacturer, the dispersion of Baytubes on a polymer matrix will reduce the length of crack and its propagation, which enhance the durability of the epoxy composite.

Table 1. Properties of DGEBA (DER 331).

Viscosity at 25°C (mPa•s)	11000-14000
Density at 25°C (g/ml)	1.16
Heat Deflection Temperature (°C)	111
Flexural Strength (N/mm ²)	96
Flexural Modulus (kN/mm ²)	3.0
Tensile Strength (N/mm ²)	79
Maximum elongation (%)	4.4

The specimens used on the tensile test were manufactured with shape and size specified by ASTM D-638-10, 2010 (Type I). For a thickness equals 7 or under, the distance between grips d is 115 mm, the gage length g is 50 mm and the initial cross section is 65 mm² ($w \times t$, where $w = 13$ mm is a standard dimension and $t = 5$ mm is the average thickness of the specimens manufactured) “Fig. 2”. The length overall l of the specimens is 165 mm. The DGEBA and carbon nanotubes were mixed and disposed in steel mold with the standard specimen size and cured at room temperature.

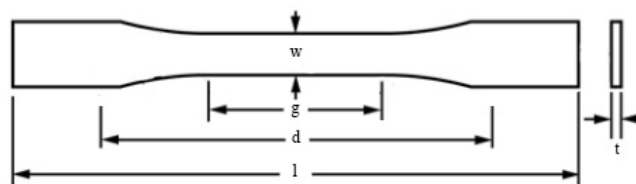


Figure 2. Standard tensile test specimen dimensions according to ASTM-D638-10

2.2 Methods

Three temperatures were pre defined: room temperature 25°C, 50°C and 75°C. For each temperature three strain rate were determined: 5 mm/min, according to ASTM-D638-10, 50 mm/min and 0,5 mm/min. Those strain rates were determined as 10% more and 10% less respectively than the standard strain rate (Reis, *et al.*, 2012).

The tensile test at 25°C were performed on a Shimadzu® AG-X universal testing machine “Fig. 3a”. For the others two temperatures an EMIC 5kN universal machine with a thermostatic chamber was used “Fig. 3b”. Five specimen were performed at a given strain rate for each temperature, total of 45, as a standard procedure (ASTM D-638-10, 2010).

After the performances, it was calculated the mean curve for each strain rate at each temperature and determined the modulus of elasticity and strength.

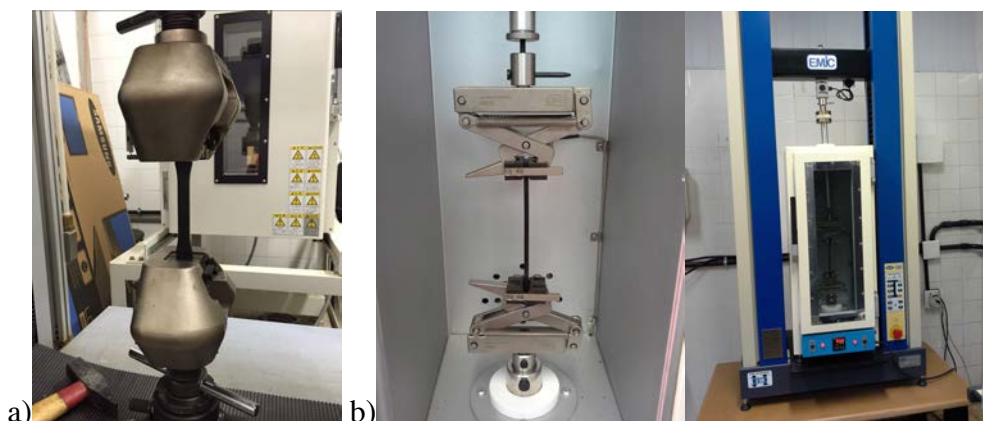


Figure 3. a) Tensile test at 25°C performed on a Shimadzu® AG-X; b) EMIC machine used to performed tensile test for 50°C and 75°C.

3. RESULTS AND DISCUSSION

The mean curves for each test are illustrated in “Fig. 4”; they were defined until the elastic limit since for the tests at 50°C and 75°C, after a while inside the oven, the material changed its linearity and the curves were too complex to analyze. Then the ultimate strength is not represented on these curves, but it is shown in “Tab. 2”.

At room temperature the curve is linear for any strain rate. As the temperature increase, the curves become unstable. At 75°C the tests at 5 mm/min resulted on a mean curve slightly lower than the tests at 0.5 mm/min. But the ultimate strength increase with higher strain rate as it was expected (“Tab. 2”).

Analyzing “Tab. 2” and “Tab. 3”, it is observed that the ultimate strength and Young’s modulus decrease with temperature and increase with strain rate, which confirms the dependence of the behavior of the composite with temperature and strain rate (Banea, *et al.*, 2011).

Table 2. Ultimate strength in MPa

	25°C	50°C	75°C
0.5 mm/min	28.25	8,03	1,03
5.0 mm/min	29.28	17,97	1,82
50,0 mm/min	31.05	18,37	2,19

Table 3. Young’s Modulus in GPa

	25°C	50°C	75°C
0.5 mm/min	2.4	1.3	0.070
5.0 mm/min	2.6	1.5	0.056
50,0 mm/min	2.8	2.1	0.269

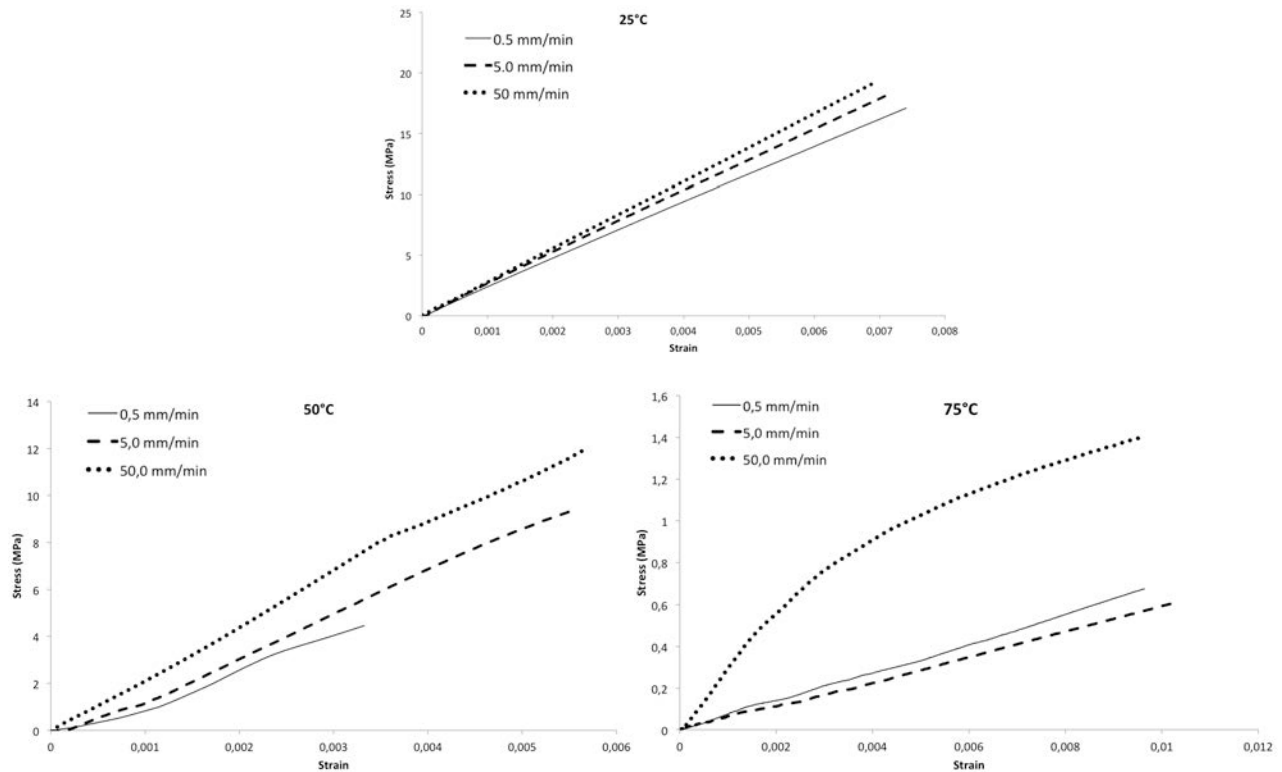


Figure 4. Top: mean curves of tests at 25°C for 0.5 mm/min, 5.0 mm/min and 50 mm/min; bottom left: mean curves of tests at 50°C for each strain rate; bottom right: mean curves of tests at 75°C for each strain rate.

The stress-strain curve showed on “Fig. 5” illustrates how this composite is influenced by temperature. When grouping all the curves above in a single chart, at 75°C the modulus of elasticity is so low that the strength could be mistaken by a constant. In fact, during the tensile tests the material was starting to melt, especially in low strain rate (0.5 mm/min), because the specimen stayed longer inside the oven, then the shape of the specimen had a slightly bent after rupture as in “Fig.6”. The difference on stiffness between the curves of 50°C and 25°C is lower than the curves of 75°C compared with 50°C, which suggest that the composite has non-linear behavior as a function of temperature. An analytical modeling would be appropriate to verify this dependence.

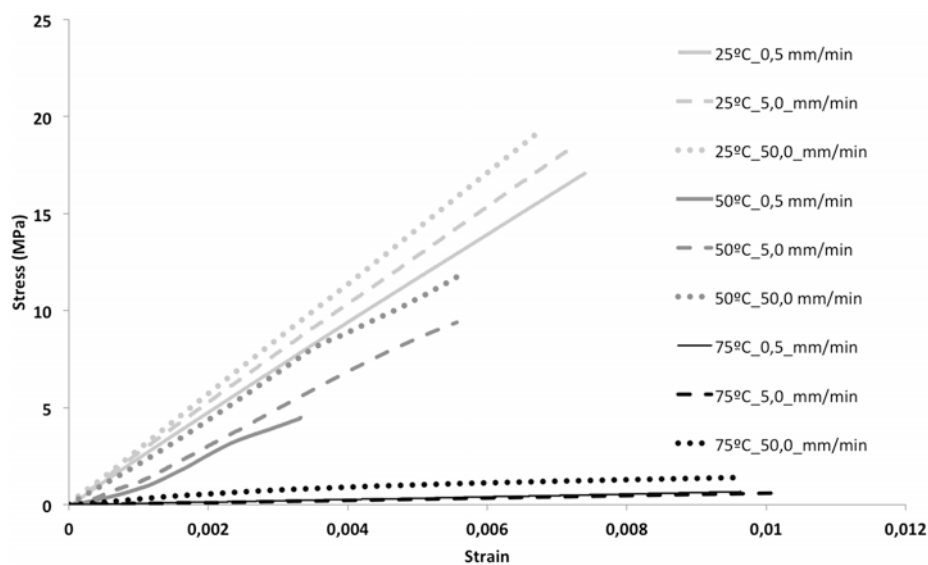


Figure 5. Mean curves of the tensile test.



Figure 6. Curved specimen after a test.

4. CONCLUSION

The effect of temperature and strain rate on the behavior of mechanical properties of the DGEBA adhesive reinforced with carbon nanotubes was observed. The response to a range of temperature (25°C, 50°C and 75°C) and strain rate (0.5, 5.0, 50.0 mm/min) was experimentally measured during tensile tests, showing a decrease of Young's modulus and ultimate strength with temperature, but an increase of these properties with strain rate. The results show that the mechanical properties of the composite are affected by the strain rate and strongly by the temperature, suggesting that this dependence is not linear. It is desirable to develop analytical expressions in future work to observe this dependence and compare the experimental results with predicted ones.

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6. RESPONSIBILITY NOTICE

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